

U.S. Department of Transportation

National Highway Traffic Safety Administration

# Analysis of Electronic Control Unit and Accelerator Pedal Mechanism Components Damaged During EMC Testing

February 2011

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## TABLE OF CONTENTS

1.0	Introduction	l
2.0	ECM Failure	2
2.1	Vehicle Detail	2
2.2	Description of Testing and Failure	2
3.0	APM Sensor Failure	5
3.1	Vehicle Detail	5
3.2	Description of Testing and Failure	5
Appe	ndix A: Denso Investigation Final Report on IC Failure Date November 5, 2010	3
Apper 01M2	ndix B: Denso Investigation Final Report on APM Sensor Failure (production date 1) Dated October 20, 2010	5
Appe	ndix C: Denso Investigation Final Report on APM Sensor Failure (production date	
03H2	0) Dated October 20, 2010	5

### 1.0 Introduction

During the Electro-Magnetic Compatibility (EMC) testing conducted by a team of NASA and NHTSA staff as part of the Toyota Unintended Acceleration (UA) study certain Electronic Throttle Control (ETC) system component failures were experienced. As discussed below, none of the component failures resulted in UA, nor was there any evidence that failures of this type were occurring in the field, and all the failures occurred under conditions unlikely to occur in consumers' use of the vehicle. For these reasons, the extent to which the failures were a result of EMC effects, component susceptibilities, the test setup/method employed, or a combination of these, was not fully evaluated by the team.

In one case the failed ETC component, an electronic control module (ECM) resulted in an engine stall (or a failure of the engine to start). In the other component failures, involving accelerator pedal mechanisms (APM), these caused the engine to remain at idle regardless of the accelerator pedal position. The failed components were subsequently evaluated by the component supplier, Denso Corporation and its subsidiary Denso Manufacturing Tennessee, with oversight provided by NHTSA staff. A description of the vehicles under test, the testing that was being performed when the failure occurred, and the Denso reports produced for the failed component are provided below.

### 2.0 ECM Failure

#### 2.1 <u>Vehicle Detail</u>

Model Year (MY) 2004 Toyota Camry XLE w/V6 1MZ-FE engine (Vehicle 14C). The vehicle was the subject of NHTSA Vehicle Owner Questionnaire ODI number 10321093<sup>1</sup>

### 2.2 Description of Testing and Failure

In July 2010 the above vehicle was being tested in an anechoic EMC test chamber operating on a dynamometer between 30 and 35 mph. The test environment of interest was in the frequency range from 144 MHz to 160 MHz, and the power level was up to a maximum of 250 volts/meter<sup>2</sup>. During the testing the vehicle was observed to slow down and eventually stall when exposed to high radio frequency (RF) energy<sup>3</sup>, and warning lights were noted to be illuminated on the instrument panel.

The testing was stopped and the vehicle was interrogated using a Toyota provided diagnostic tool called a TechStream Lite, a PC based device. The TechStream connects to the vehicle's diagnostic link connector (DLC) via a USB device, called a Mongoose cable, which allows the PC to communicate with the ECM and other vehicle systems. The interrogation showed that engine diagnostic trouble codes (DTCs) P0346, P0717, P2241, B2799, P0346, P0353, P0356 and ABS/VSC/TRAC DTCS C1201, C1203, C1224 had been stored.

In an attempt to collect additional information on the DTCs and engine performance issues experienced during the testing, the team elected to conduct additional EMC testing while the

<sup>&</sup>lt;sup>1</sup> A public copy of the report is available at <u>http://www-odi.nhtsa.dot.gov/complaints/</u>.

<sup>&</sup>lt;sup>2</sup> The signal was being modulated using a 50% duty cycle square wave at 1 kHz.

<sup>&</sup>lt;sup>3</sup> The vehicle speed could be modulated (slowed) gradually by adjusting the power level of the RF. A number of tests were run at various power levels to characterize this behavior, all in the 144 to 160 MHz frequency range.

TechStream device was connected to the vehicle, since this would allow various ECM data parameters to be monitored.

To accomplish this the PC was located outside of the test chamber (in a Faraday cage for EMC protection). The Mongoose cable was routed between the vehicle and the PC, and an optical USB coupling device was utilized between the Mongoose cable and the PC. The optical coupling device required power at the Mongoose cable connection to provide 5Vdc to the Mongoose cable (this power normally comes from the PC USB port). As a result of this setup the Mongoose cable, the powered end of the optical USB coupling cable, and the 5Vdc power supply wires, all of which were routed in the vehicle and test chamber, were exposed to the RF environment during conduct of the test. The Mongoose interface, the 5Vdc power supply cable, and the powered end of the optical USB coupler were all wrapped in a double layer of aluminum foil to provide shielding from the RF energy.

As the testing proceeded the TechStream began exhibiting difficulty communicating with the ECM and at some point the engine stalled and could not be restarted<sup>4</sup>; at this point the TechStream lost all communication with the ECM. A replacement ECM was installed in the vehicle as a test to confirm the ECM had failed. It is important to note that subsequent to this failure no other vehicles were EMC tested with a TechStream device connected to the DLC, and none of the other vehicles tested in equivalent RF environments experienced an ECM failure.

In August 2010 NHTSA staff hand carried the failed ECM to a Denso facility located in Maryville, TN for additional assessment. Through testing and component swapping, which was witnessed by NHTSA staff, Denso determined that a specific integrated circuit (IC) component

<sup>&</sup>lt;sup>4</sup> The engine would crank over with the starter motor but would not start and run on its own.

known as the sub-microprocessor (or monitor CPU) had failed. The failed component was removed and replaced with a known good IC. NHTSA retained possession of the repaired ECM and failed IC after the Denso assessment. The ECM was subsequently returned to the EMC test team for assessment in the above vehicle and the team confirmed it was functioning correctly after replacement of the single component.

In September 2010, after discussion by staff involved in the EMC testing, the failed IC was sent to Denso's Electronic QA department in Japan. Their assessment, which included destructive analysis by the IC component manufacturer, determined that the IC's flash memory was damaged possibly due to high current produced by abnormal electric fields. In November 2010 Denso produced a report which is attached below as Appendix A.

### 3.0 APM Sensor Failure

#### 3.1 <u>Vehicle Detail</u>

MY 2007 Toyota Camry XLE w/V6 2GR-FE engine (Vehicle 12C). The vehicle was the subject of NHTSA Vehicle Owner Questionnaire ODI number 10319201<sup>5</sup>

### 3.2 Description of Testing and Failure

In July and August 2010 the EMC team began evaluating observations made by Dr. Todd Hubing of Clemson University as discussed in a July 2010 presentation to the Electronic Vehicle Controls and Unintended Acceleration committee of the National Academy of Sciences<sup>6</sup>. Dr Hubing studied the effects of RF currents coupled to sensor wiring of the accelerator pedal mechanism (APM) that could, at certain frequencies and power levels, cause the engine to accelerate without driver input. Dr Hubing did not provide evidence of a mechanism, or that such effects were actually occurring in the consumer's use of the vehicle, hence the effects are considered only theoretical in nature. Dr. Hubing's work, including the frequencies and power levels used, formed the basis of evaluation conducted by the EMC team.

The APMs used in Toyota's Electronic Throttle Control System have both a primary and a (redundant) secondary accelerator pedal position sensing device that is referred to as an APP sensor, or just an APP. Each sensor circuit has connections for a power line, a return line (ground), and an output signal line, so six wires are used to connect the APP directly to the ECM<sup>7</sup>. Two technologies were used for the APP sensors; potentiometer based sensors<sup>8</sup> were

<sup>&</sup>lt;sup>5</sup> A public copy of the report is available at <u>http://www-odi.nhtsa.dot.gov/complaints/</u>.

<sup>&</sup>lt;sup>6</sup> The presentation is available at <u>http://onlinepubs.trb.org/onlinepubs/ua/100701hubing.pdf;</u> slide 17 discusses specific testing that was evaluated.

<sup>&</sup>lt;sup>7</sup> Further technical details of the APP sensor, wiring, and signal characteristics can be found in the main NASA and NHTSA reports available at <u>http://www.nhtsa.gov/UA</u>.

used on MY 2002 to 2006 while Hall Effect (HE) based sensors were used on MY 2007 and later<sup>9</sup>. The Camry HE APP assemblies were manufactured by two suppliers, CTS and Denso<sup>10</sup>.

For these tests an inductive coupler was used to introduce RF signals into the APP wiring. The coupler can encircle one or more APP wires and then inject RF energy inductively, i.e., without electrically contacting the wire(s). In testing conducted by the team, the Denso HE based APP exhibited a characteristic that was not observed while testing the other APP type. Specifically, when certain APP wires were encircled by an inductive coupler<sup>11</sup>, and exposed to specific frequency and power levels, the engine speed would increase without APM movement. NHTSA notes that it is unaware of any real-world evidence indicating that this characteristics has occurred in service, however it could result in UA if it were to somehow occur.

In the testing conducted on the Denso HE APM, engine speed increases could be observed when the two power supply wires, or the two signal output wires, or the signal output and power wires together were exposed to RF energy via the inductive couple. For instance, in one test conducted at 100 kHz and 100 dB-micro-amps of power, an increase in the APP output signals was observed leading to a throttle opening (without APM application). The testing showed that this outcome only occurs if two or four of the six wires (power and/or signal) in the APM wire bundle are exposed to RF energy<sup>12</sup>; if all six leads are exposed to RF energy together, then no effects are noted. Additionally no such effects were seen for the testing conducted on potentiometer-based or CTS supplied HE APMs.

<sup>&</sup>lt;sup>8</sup> Potentiometer sensors utilize a mechanical contact device, known as a wiper that moves against a resistive element electrically situated between the 5  $V_{DC}$  rail and ground. These sensors have high output impedance.

<sup>&</sup>lt;sup>9</sup> HE sensors are non-contacting devices that improve durability and have low impedance output characteristics.

<sup>&</sup>lt;sup>10</sup> The CTS pedal makes use of a HE IC manufactured by Melexis, while the Denso pedal uses a Micronas device.

<sup>&</sup>lt;sup>11</sup> No engine speed change occurs if all of the APP wires are encircled by the inductive coupler.

<sup>&</sup>lt;sup>12</sup> Note that certain aftermarket devices (e.g. cruise control systems, remote start devices) that connect directly to the APP power or output signals may provide a pathway for EMI into the APM circuitry.

During a portion of the Denso APM testing which involved RF exposure of the two signal return lines only, damage to the sensor occurred and there was a loss of signal output. In this situation a DTC was set, the engine returned to the idle state, and application of the accelerator pedal had no effect on engine speed. Two Denso APMs that failed in this manner were subsequently returned to Denso for analysis. Denso's October 2010 analysis reports for each failed APM, which showed that a bonding lead for the sensor return circuit had been damaged through electrical overstress, are included as Appendix B and C below. Appendix A: Denso Investigation Final Report on IC Failure Date November 5, 2010

DENSO

5,Nov,2010

TO : DENSO MANUFACTURING TENNESSEE ELECTRONIC DIVISION QA FROM : DENSO CORPORATION ELECTRONICS QA

### **INVESTIGATION FINAL REPORT**

CC. DNJP:ELECTRONICS ENG.DEPT.1 DESIGN SECT.1 ELECTRONICS QA DEPT. PRODUCT QA CENTER 1 QUALITY CONTROL DEPT.

> ELECTRONICS QUALITY ASSURANCE DEPT. PURCHASED PARTS QA

12010 NOV WRITTEN BY en Kasahara Kenji Kasahara CHECKED BY Hiroyuki Tanizawa APPROVED BY 5.NOT.

Masao Soumiya

9

1/6

DENSO report the analysis result depend on IC supplier report .

#### Monitor CPU Preliminary Investigation result

(1) Componen	t Information
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Part Name	: UPD76F0004GD(a1)-24-5GD-CAR
Lot No.	: 0332MX033 (Product on 2003, week32)
Supplier name	: RENESAS ELECTRONICS CORPORATION

#### (2) I - V characteristic check : No abnormality was observed



(3) X-Ray Analysis : No abnormality was observed



(4) FLASH Memory Writing check : No abnormality was observed LSI tester : Can write the data correctly in FLASH Memory area

FLASH programmable tool : Can write the data correctly in FLASH Memory area

#### (5) FLASH Memory Reading check : Abnormality was observed

Can not read out the data from FLASH Memory at high speed frequency .

(Speed marginal failure of reading FLASH memory)



(6) Presumption of Defective area

The supplier is presuming that there will be defective point at the circuit relating FLASH reading in FLASH macro area .

So they are going to do further analysis in this area .



#### Monitor CPU Investigation result



#### (2) OBELISCH check : Abnormality was observed

The supplier performed OBELISCH analysis at the low marginal memory cell in FLASH

macro area , and confirmed the abnormal emission spot in the sense AMP circuit .

\*OBELISCH (Optical Beam induced Logic State Change)

: OBELISCH is one of the analysis method that can localize the defective point by scanning IR-laser with using LSI tester & IR OBIRCH machine .

[OBELISCH image]





#### (3) TEM check : Abnormality was observed

The supplier performed TEM analysis at the above emission point (N-ch Transistor), and confirmed the abnormality ( delamination & Void ) .

\*TEM (Transmission Electron Microscope)

: TEM is a microscopy technique whereby a beam of electrons is transmitted through an ultra thin specimen , interacting with the specimen as it passes through .









Above physical analysis revealed that the resistive impedance between G1 drain and G2 source goes up and it introduced malfunction of FLASH memory reading at high frequency.

No Delamination, Void



The supplier assumed that the electrical characteristics of this transistor should be changed , for example , lon current should be smaller and threshold voltage should be higher than normal .

(4) FTA (Failure Tree Analysis)



#### (5) Conclusion

The supplier found defective points of die, and these were sense Amp circuit N-ch MOSs (G1 & G2).

These points had delamination and voids, and became high resistive characteristic.

This high resistive characteristic of these transistors can explain the malfunction of

FLASH memory reading at high speed frequency.

The supplier could not find manufacturing fault .

It is assumed that this abnormality occurred for the reason of the following.

•A high current flowed into the sense AMP circuit under the abnormal electric field, and overheated.

·The delamination and voids occurred.

**Appendix B:** Denso Investigation Final Report on APM Sensor Failure (production date 01M21) Dated October 20, 2010

# DENCO

/ <u>SO</u>			
Final repo	ort		
TO:National Highway Traffic	Safety	Administration	
SENSOR ASSEMBLY,	ACCELE	RATOR PEDAL	
INVESTIGATIO	N REPC	<u>DRT</u>	
Part Name: SENSOR ASSY, ACCEL	ERATOR	PEDAL	
Customer Part Number: 78110-33020 (DN:19	8800-719	0)	
Investigation part No 2 ( Pro	duction o	late · 01M21)	
	DENSO CO SYSTEM CONTR	RPORATION	
	Checked	N.Kihara	
		K.Horie	
	Approved	T Hamaoka	
ISSUE DATE:	DENSO CO	PRPORATION	
<u>ISSUE DATE:</u> 20.Oct.2010	DENSO CC system contr Written	RPORATION ROL CONPONENTS QA DEPT4.	
<u>ISSUE DATE:</u> 20.Oct.2010	DENSO CC system contre Written Checked	PRPORATION ROL COMPONENTS QA DEPT4. T.Kobayasi	
<u>ISSUE DATE:</u> 20.Oct.2010	DENSO CC system contre Written Checked	PRPORATION ROL COMPONENTS QA DEPT4. T.Kobayasi S.Nakano	
<u>ISSUE DATE:</u> 20.Oct.2010	DENSO CC system contr Written Checked Checked	PRPORATION ROL CONPONENTS QA DEPT4. T.Kobayasi S.Nakano K.Kato	
<u>ISSUE DATE:</u> 20.Oct.2010	DENSO CC SYSTEM CONTR Written Checked Checked Approved	PRPORATION ROL CONPONENTS QA DEPT4. T.Kobayasi S.Nakano K.Kato T.Sakai	

1. Inv	estigation parts	Data		
No.	Customer.P/N	Denso .P/N	Production date (DENSO)	Content
2	78110-33020	198800-7190	21.Jan.2010 (01M21)	APM Component failures during NHTSA testing.

#### 2. SENSOR ASSY, ACCELERATOR PEDAL Investigation Result

Item	Result	Page
1) Appearance	No abnormality is found.	3/10
2) Operation feeling check	No abnormality is found.	3/10
3) Performance	Abnormalities are observed in Vpa1 and Vpa2 other than the pedal effort.	3/10
4)Output waveform	Abnormalities are observed in Vpa1 and Vpa2.	4/10
5) Pedal effort	No abnormality is found.	4/10
6) X-ray	Abnormal IC is confirmed.	5/10
7) Disassembly	We can see that it smells melting resin.(Sensor cover IC section )	5/10
8) IC Investigation	A broken wire bonding is found.	6/10,7/1

#### 3. Conclusion

Investigation part No.2(01M21)

As a result of the investigation, we found abnormalities in the electrical characteristics other than the pedal effort. During disassembly check, we identified the cause of the defect, based on the results of the broken IC wire bonding and the IC replacement check.

The broken IC wire bonding caused an abnormality in the electrical characteristics.

Therefore we asked the IC supplier (overseas maker) for analysis.

We have never experienced the IC wire bonding failure in the SENSOR ASSY, ACCELERATOR PEDAL before. We would appreciate it if you could let us know your test conditions.

<Results of the investigation carried out by the IC supplier> Through the investigation, at both VPA 1 and VPA2, we identified the wire bonding molten which are used to make interconnections between IC and terminals. We identified molten metal wires (AI) and the discoloration at several areas including bond pads. Therefore we came to a conclusion that excessive electrical overstress was applied to the IC through the external sources. The electrical overstress (EOS) may have caused the IC to break.

	Over	rall figure		Bas	e side	
	Connector	-A view	M.	X		
significar	it scratches and d	leformation are fo	ound in the sensor	lo significant scratches a	and deformation are	e found.
	Co	nnector	Vehic	le installation side	A	view
.(		1 A A			T	
No sign	ificant scratches	and deformation	on are found.	ificant scratches and	No foreig	n material
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ethod>S S sult> • · · · · · · · · · · · · · · · · · ·	Teeling check tep 1 : The re tep 2 : The p The pedal is m ince at roo a found abnor ITEMS TOLTAGE TOLTAGE TOLL-CLOSE TOLTAGE Y AT 25± 10°C) ICE IN OUTPUTS	turned part is     edal is repeate     noved smoothly     m temperature     malities in the         √pal	clamped with bolts to a jig. edly moved to the full-open po y. e: e electric characteristics (V sPEC 0.75 - 0.89V +0.040V 0.29*+0.50/-0.16* ±0.040V 10.060V ±0.120V ±0.120V ±0.120V ±0.120V ±0.120V ±0.120V ±0.120V	pat and Vpa2) other           RESULT           Vpa1         0.065           0.000         0.000 </td <td>Description by hat           than the pedal e           at RT)           Vpa2           0.000           0.000           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000</td> <td>nd. stfort. JUDGMEN NG NG NG NG NG NG NG NG NG N</td>	Description by hat           than the pedal e           at RT)           Vpa2           0.000           0.000           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           -           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000           0.000	nd. stfort. JUDGMEN NG NG NG NG NG NG NG NG NG N
ethod>S Sult> - S sult> - We - We OUTPUTA AT FULLC REPRODE VOLTAGE OUTPUTA REFINDING P LINEARIT OUTPUTA (LINEARIT DIFFEREN (25±10°c) See Fig-1	Teeling check tep 1 : The re tep 2 : The p The pedal is m ince at roo a found abnor ITEMS (OLTAGE COSE CO	turned part is edal is repeate noved smoothly om temperature malities in the y≠a1 0,*~ 2* 2*~ 4* 4*~10* 10*~ 5.5* 0*~5* 5*~12* 12*~ 20* PRESSING RELEASING	clamped with bolts to a jig. edly moved to the full-open po y. e: e electric characteristics (V	pa1 and Vpa2) other           RESULI           Vpa1           0.065           -           5.000           0.000	Description         by has           than the pedal e         e           at RT)         Vpa2           Vpa2         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.000         -           0.1624         9           92         -           09         -           Ugation parts:20.9N ()         -           Ugation parts:7.0N ()         -	nd. affort. JUDGMEN NG NG NG NG NG NG NG NG NG N
ethod>S Sult> • S sult> • S erforma • We output At FULL-O REPRODU VOLTAOE OUTPUT UNEARIT UNEARIT DIFFEREN (25±10°C) See Fig-1 PEDAL EFFORI	Teeling check           itep 1 : The reference           itep 2 : The p           The pedal is management           Ince         at roo           e found abnor           Interms	sturned part is edal is repeate noved smoothly im temperature malities in the vial $v_{i=1}$ v	clamped with bolts to a jig. edly moved to the full-open porture e electric characteristics (V 0.75 ~ 0.89V + 0.040V 0.29*+0.50/-0.18* ± 0.040V 10.060V ± 0.120V ± 0.120V ± 0.135V Fig-1 ± 30% OF INITIAL VALUE(N · m) (SPEC; 14.0~25.9N · m) ± 33% OF INITIAL VALUE(N · m) (SPEC; 5.3~9.9N · m)	pa1 and Vpa2) other           Pa1 and Vpa2) other           RESULT           Vpa1           0.065           -           5.000           0.005           -           5.000           0.005           -           5.000           0.000	ese position by har than the pedal e at RT Vpa2 Vpa2 - 0.000 0.000 -0.745 -1.624 9 9 9 10 10 10 10 10 10 10 10 10 10	nd. JUDGMEN NG NG NG NG NG NG NG NG NG N
ethod>S sult> · S sult> · · We · We · We OUTPUT\ AT FULLC REPRODE VOLTAGE OUTPUT\ RIBING P LINEARIT OUTPUT\ (LNEARIT DIFFEREN (25±10°c) See Fig-1 PEDAL EFFORI	Teeling check tep 1 : The re tep 2 : The p The pedal is m ince at roo a found abnor ITEMS (OLTAGE LOSE TOTAGE ONT (Vpet) (OF VAT 25±10°C) ICE IN OUTPUTS IO FULL -OLOSE INT, (Vpet) ICE IN OUTPUTS IO FULL -OLOSE INT, (Vpet) ICE IN OUTPUTS	turned part is edal is repeate noved smoothly om temperature malities in the vpa1 0,*~ 2* 2*~ 4* 4*~10* 10*~ 15.5* 0*~5* 5*~12* 12*~ 20* PRESSING RELEASING PRESSING	clamped with bolts to a jig. edly moved to the full-open po y. e: e electric characteristics (V sPEC 0.75 - 0.89V + 0.040V 0.29*+0.50/-0.18* ± 0.040V 0.29*+0.50/-0.18* ± 0.040V ± 0.120V ± 0.120V (SPEC; 14.0~25.9N·m) ± 30% OF INITIAL VALUE(N·m) (SPEC; 2.2~9.9N·m) ± 30% OF INITIAL VALUE(N·m) (SPEC; 2.2~9.9N·m)	pa1 and Vpa2) other           RESULT           Vpa1           0.065           -           5.000           0.005           -           5.000           0.001           0.002           0.003           0.004           0.005           0.001           0.002           0.002           0.003           0.004           0.005           0.005           0.000           0.001           0.002           0.003           0.004           0	at RT)         Vpa2           0.000         0.000           0.000         0.000           0.000         - <t< td=""><td>nd. JUDGMEN NG NG NG NG NG NG NG NG NG NG NG NG NG</td></t<>	nd. JUDGMEN NG NG NG NG NG NG NG NG NG NG NG NG NG















### 4-5 : Remarks

Through the investigation, at both VPA 1 and VPA2, we identified the wire bonding molten which are used to make interconnections between IC and terminals.

We identified molten metal wires (AI) and the discoloration at several areas including bond pads. Therefore we came to a conclusion that excessive electrical overstress was applied to the IC through the external sources. The electrical overstress (EOS) may have caused the IC to break. **Appendix C:** Denso Investigation Final Report on APM Sensor Failure (production date 03H20) Dated October 20, 2010

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тшатер	on	
TO:National Highway Traffic	Safety Ad	dministration
SENSOR ASSEMBLY,	ACCELER	ATOR PEDAL
INVESTIGATIO	N REPOR	T
ustomer art Number: 78110-33020 (DN:19	98800-7190)	
Investigation part No.1(Pro	oduction dat	te : 03H20)
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<u>1. Deta</u>	ails of investiga	ation part		
No.	Customer.P/N	Denso .P/N	Production date (DENSO)	Content
1	78110 33020	198800 7190	20.Mar.2006 (03H20)	APM Component failures during NHTSA testing.

#### 2. SENSOR ASSY, ACCELERATOR PEDAL Investigation Result

ltem	Result	Page
1) Appearance	*Connector crack is confirmed.	3/7
2) Operation feeling check	No abnormality is found.	3/7
3) Performance	Abnormalities are observed in Vpa1 and Vpa2 other than the pedal effort.	3/7
4) Output waveform	Abnormalities are observed in Vpa1 and Vpa2.	4/7
5) Pedal effort	No abnormality is found.	4/7
6) X-ray	Abnormal IC is confirmed.	5/7
7) Disassembly	The resin has melted. (Sensor cover IC section)	5/7
8) IC Investigation	A broken wire bonding is found.	6/7

\*Connector crack

The appearance and the performance are 100% checked so it is possible to detect nicks and cracks in our production process. As a result of the investigation, we presumed that the deformation occurred after shipping from our plant.

#### 3. Conclusion

Investigation part No.1(03H20)

As a result of the investigation, we found abnormalities in the electrical characteristics other than the pedal effort. During disassembly check, we found that the wire bonding in the IC got cut off.

The broken IC wire bonding caused an abnormality in the electrical characteristics.

Therefore we asked the IC supplier (overseas maker) for analysis.

We have never experienced the IC wire bonding failure in the SENSOR ASSY, ACCELERATOR PEDAL before. We would appreciate it if you could let us know your test conditions.

<Results of investigation carried out by IC supplier > Si chip of Vpa1 came off when disassembling, Si chip got stuck in the molded resin part. We cannot continue to carry out further investigation. However, we confirmed the discoloration of the Vpa2 platform. Therefore we came to a conclusion that excessive electrical overstress was applied to the IC through the external sources. The electrical overstress (EOS) may have caused the IC to break.

	Overall f	faure			Base side	
Co	nnector	A view	1		Since Care	0
icant scra	tches and defor and pedal r	mation are fou od part	ind in the sensor	No significant scrate	ches and deforma	tion are found
	Conne	ctor	Ve	hicle installation side		A view
C			Crack			
	Cracks are	e found.	No si	gnificant scratches ar	nd N	lo foreign mat
• The p	: The peda bedal is move at room te	i is repeated ad smoothly emperature:	Aly moved to the full-open . A sticking pedal is not for	position from the fu	III-close position	by hand.
• The p • The p • mance • We fou	: The peda cedal is move at room te nd abnorma итемз	is repeated ad smoothly emperature: alities in the	Aly moved to the full-open . A sticking pedal is not for electric characteristics	position from the fu und. (Vpa1 and Vpa2) ( RESULT Vra1	other than the	n by hand. pedal effort 
• The p mance We fou	: The peda cedal is move at room te ind abnorma итема остлове Lose	I is repeated ad smoothly. Intresture: Intres in the	aly moved to the full-open . A sticking pedal is not for electric characteristics arco 0.75~0.89V	position from the fu and. (Vpa1 and Vpa2) ( RESULT Vpa1 0.031	other than the	реdal effort JUDOMENT NG
• The p • T	: The peda cedal is move aat room te ind abnorma итемо остлое сов сов сов сов сов сов сов сов сов сов	I is repeated and smoothly imperature: lities in the	aly moved to the full-open . A sticking pedal is not for e electric characteristics orco 0.75~0.89V ±0.040V 0.29°-0.60/-0.16°	position from the fu und. (Vpa1 and Vpa2) ( RESULT Vpa1 0.031	other than the (#RT) Vpa2	pedal effort JUDOMENT NG NG
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Step 2 • The p mance We fou outputv ATFUL-C REPRODU VOLTAGE , DUTPUTV RIBING PC LINEARITY DUTPUTV	: The peda cedal is move and abnorma items outrace cost cost cost cost cost cost cost cost	$\theta_{1}$ is repeated and smoothly. Introduces in the VPa1 $\theta_{1}^{*}\sim 2^{*}$ $\frac{\theta_{1}^{*}\sim 2^{*}}{2^{*}\sim 4^{*}}$	aly moved to the full-open           . A sticking pedal is not for           electric characteristics           arcc           0.75~0.89V           ±0.040V           0.29*-0.50/-0.16*           +0.040V           ±0.040V           0.29*-0.50/-0.16*           +0.040V	position from the full           und.           (Vpa1 and Vpa2) (           RESULT           Vpa1           0.031           -           5.000           0.000	other than the (#RT) Vpa2	Pedal effort
Step 2 • The p mance We fou outputv atfull-ci REPRODU voltage outputv RIBINO PC LINEARITY DUTPUTV (LINEARITY	: The peda cedal is move at room te ind abnorma items outrage cibility of out at full-close outrage outrage outrage (AT25±10°C)	$\theta_{i}^{*} \sim 2^{*}$ $\theta_{i}^{*} \sim 2^{*}$ $\theta_{i}^{*} \sim 2^{*}$ $\frac{\theta_{i}^{*} \sim 2^{*}}{2^{*} \sim 4^{*}}$ $\frac{10^{*}}{10^{*}}$ $\frac{10^{*}}{10^{*}}$	aly moved to the full-open         . A sticking pedal is not for         electric characteristics         orcc         0.75~0.89V         ±0.040V         0.25*0.50/-0.16*         +0.040V         ±0.060V         ±0.050V         ±0.050V	position from the full           und.           (Vpa1 and Vpa2) (           RESULT           Vpa1           0.031           -           5.000           0.000           -0.745           -1.945	other than the (@RT) Vpa2 - 0.000 -0.745 - 0.000	Pedal effort
Step 2 • The p mance We fou outputv atfull-ci REPRODU voltage, outputv RISINO PC LINEARITY outputv LINEARITY outputv LINEARITY DIFFEREN	: The peda cedal is move at room te and abnorma items outrace cost cost cost cost cost cost cost cost	$\theta_{i}^{*} \sim 2^{*}$ $\theta_{i}^{*} \sim 2^{*}$ $\frac{\theta_{i}^{*} \sim 2^{*}}{2^{*} \sim 4^{*}}$ $\frac{\theta_{i}^{*} \sim 2^{*}}{10^{*} \sim 10^{*}}$ $\frac{\theta_{i}^{*} \sim 2^{*}}{10^{*} \sim 15^{*}}$	aly moved to the full-open           A sticking pedal is not for           electric characteristics           arcc           0.75~0.89V           ±0.040V           0.29*-0.50/-0.16*           +0.040V           ±0.050V           ±0.050V           ±0.120V           ±0.135V	position from the full           und.           (Vpa1 and Vpa2) (           RESULT           Vpa1           0.031           -           5.000           0.000           -0.745           -1.821	other than the (#RT) Vpa2 - - 0.000 -0.745 -1.609 517	Pedal effort JUDOMENT NG NG NG NG NG
Step 2 • The p mance We four outputv ATFULCCI REPRODU VOLTAGE, OUTPUTV RISINO PC LINEARITY OUTPUTV (LINEARITY DIFFEREN (25±10°C)	: The peda cedal is move and abnorma rremo outrace cose cose cose cose cose cose cose co	θ: repeated           ad smoothly.           emperature:           lities in the           Vpa1           Vpa1           0:~.2*           2*~4*           4*~.10*           10*~.15*           5*~.12*	aly moved to the full-open . A sticking pedal is not for pelectric characteristics 0.75~0.89V ±0.040V 0.29°+0.50/-0.16° +0.040V ±0.050V ±0.120V ±0.120V ±0.135V Eig 4	position from the full           (Vpa1 and Vpa2) (           RESULT           Vpa1           0.031           -           5.000           0.000           -0.745           -1.621           -0.6	other than the (at RT) Vpa2 - 0.000 -0.745 -1.609 517	Pedal effort JUDOMENT NG NG NG NG NG NG NG NG
Step 2 • The p mance We four outputv Atfull-ci REPRODU voltage, outputv voltage, outputv (LINEARITY outputv (LINEARITY DIFFEREN (25±10°c) See, hig-1	: The peda cedal is move and abnorma intems outrage cost cost cost cost cost cost cost cost	θ <sub>1</sub> is repeated           ed smoothly.           emperature:           dities in the           VPa1           VPa1           0*~2*           2*~4*           4*~10*           10*~15.9*           0*~5*           5*~12*           12*~20*	aly moved to the full-open . A sticking pedal is not for electric characteristics 0.75~0.89V ±0.040V 0.29°-0.50/-0.16° ±0.040V ±0.040V ±0.040V ±0.040V ±0.040V ±0.135V Fig-1	position from the fu Ind. (Vpa1 and Vpa2) of RESULT Vpa1 0.031 - 5.000 0.000 -0.745 -1.621 0.02 -0.000 -0.745 -0.000 -0.745 -0.000 -0.000 -0.745 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000 -0.0000	other than the           (a(RT)           Vpa2           -           0.000           -      <	Pedal effort JUDOMENT NG NG NG NG NG NG NG NG
Step 2 • The p mance We four outputv ATFULC: REPRODU VOLTAGE, OUTPUTV RISING PC LINEARITY OUTPUTV (LINEARITY DIFFEREN (25±10°c) See. Fig-1		θ <sub>i</sub> *~2*           2*~4*           4*~10*           10*~15.9*           0*~5*           5*~12*           12*~20*           PRESSING	aly moved to the full-open . A sticking pedal is not for electric characteristics 0.75~0.89V ±0.040V 0.29°-0.60/-0.16° ±0.040V ±0.040V ±0.040V ±0.040V ±0.120V ±0.135V Fig.1 ±30% OF INITAL VALUE(N·m) (SPEC :14.0~25.9N·m)	position from the fu Ind. (Vpa1 and Vpa2) of RESULT Vpa1 0.031 - 5.000 0.000 -0.745 -1.621 -0.66 -0.7% (Initiat 19 9N Inve	other than the           (a.RT)           Vpa2           -           0.000           -           0.000           -	Pedal effort JUDOMENT NG NG NG NG NG NG NG NG NG NG NG NG
Step 2 • The p mance We four outputv ATFULL-CI REPRODU VOLTAGE, OUTPUTV RISINO PC LINEARITY OUTPUTV (LINEARITY DIFFEREN (25±10°C) See. Fig-1 PEDAL EFFORT	: The peda     : The peda     : Dedal is move     at room te     ind abnorma     iTEM0     OLTAGE     CIBILITY OF OUT     AT FULL -CLOSE     (AT 25±10°C)     CE IN OUTPUTS     TO FULL -CLOSE     (at 1.55°)	0: repeated           ad smoothly.           emperature:           alities in the           Vpa1           vpa1           0:~2*           2*~4*           4*~10*           10*~15*           5*~12*           12*~20*           PRESSING           FELEADINO	aly moved to the full-open . A sticking pedal is not for pelectric characteristics 0.75~0.89V ±0.040V 0.29**0.50/-0.16* ±0.040V ±0.120V ±0.120V ±0.135V Fig.1 ±30% OF INITALVALUE(N-m) (SPEC; 14.0~25.9N-m) ±30% OF INITALVALUE(N-m) (SPEC; 61~11.3N-m)	position from the fu Ind. (Vpa1 and Vpa2) ( RESULT Vpa1 0.031 - 5.000 0.000 0.000 -0.745 -1.621 -0.6 -0.7% (Initial: 19.9N Inve -12.6% (Initial:8.7N Inve	other than the (at RT) Vpa2 - 0 000 -0.745 -1.609 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 517 518 518 518 518 518 518 518 518	Pedal effort JUDOMENT NG NG NG NG NG NG NG NG NG NG NG NG NG
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## FNSO









Si chip of Vpa1 came off when disassembling, Si chip got stuck in the molded resin part. We cannot continue to carry out further investigation. However, we confirmed the discoloration of the Vpa2 platform. Therefore we came to a conclusion that excessive electrical overstress was applied to the IC through the external sources. The electrical overstress (EOS) may have caused the IC to break.